



Application of Low Voltage Spreaders

INTERIM INSTRUCTION # AMS 2020/001

Document Control		
Author	Name: Leonard Lee Position: Senior Engineer - Networks	
Endorsed By	Name: Sandeep Magan Position: Engineering Services Manager	
Approved By *	Name: Marc Beckx Position: Manager Engineering and Project Services	
Date Created/Last Updated	21 st October 2020	

STAKEHOLDERS <i>The following positions shall be consulted if an update or review is required:</i>	
Manager Asset Services	Works Delivery Managers
Manager Safety and Wellbeing	Field Practices Coordinator
Regional Managers	EPCM Contracts Manager
Asset Managers	

1. OVERVIEW

Conductor clashing can not only cause damage to equipment, it can also impose safety risk including blackouts and bushfire. Most frequently, conductor clashing takes place as a result of inadequate clearances between adjacent conductors. For this reason, Low Voltage (LV) spreaders have historically been used in occasions where adjacent LV conductors are suspected to be too close to one another.

In-line with Horizon Power's Distribution Design Rules, any new low-voltage overhead circuit shall be built using LV ABC. LV bare conductors may still be used under exceptional circumstance. However, any new LV circuit utilising LV bare conductors must be designed to meet AS7000 without having to rely on use of LV spreaders.

The use of LV spreaders as a conductor clashing prevention strategy must therefore be limited to existing LV circuits. This document provides an interim application guide for LV spreaders.

2. APPLICATION

The application of LV spreaders on existing LV span can be considered where:

1. It has been identified as the most economically and practically justifiable option to implement. This typically involves situations where undergrounding and immediate re-conductoring with LV ABC is found to be cost prohibitive and one or more of the following apply:
 - a. The span length is in excess of 55m;
 - b. Historically there has been known clashing or the installation is within high fire risk area or an area deemed to have high-risk of clashing due to reason such as:
 - i. Heavy vegetation/overhanging trees;
 - ii. Use of dissimilar conductors on same span;
 - iii. Separation distance between LV conductors of less than 0.535m (typical separation distance between LV conductors);
 - iv. Transposition of conductors from a horizontal to a vertical arrangement.
2. Site assessment has been carried out to ensure that the associated conductors, cross-arms and poles are in good, serviceable condition

3. SIMULATION

The need for an LV spreader as well as the number of LV spreader required for a particular span can be determined by performing the necessary simulation in Poles'n'Wires. A mid-span clearance assessment shall be performed based on:

1. Mid-span separation constant of :
 - a. 0.4 in low fire-risk/non-cyclonic area or
 - b. 0.6 in any other circumstance;
2. On-site measurements of attachment points in particular for:
 - a. Scenario with least separation distance between the adjacent conductors;
 - b. Scenario with greatest potential difference (voltage) between adjacent conductors
3. Conductor with the greatest sag (where there are dissimilar conductor used within the same span);
4. Conductor temperature of 50 deg C
5. On-site verified conductor tension (recommended) or otherwise conductor tension as per the following:
 - a. For spans up to 55m:
 - i. (Old) Copper – 10% tension (7/12)
 - ii. AAC – 10% tension (7/2.75, 7/4.75, 19/3.25)
 - iii. AAAC – 7% tension (7/2.75, 7/4.75, 19/3.25)
 - b. For spans greater than 55m:
 - i. (Old) Copper – 25% tension (7/12)
 - ii. AAAC – 18% tension (7/2.75, 7/4.75, 19/3.25)

IMPORTANT: Additional assessment will be required where transposition of conductor from a horizontal to a vertical arrangement takes place – please request for assistance/review from the Standards group

4. EXAMPLE

Consider the following scenario:

1. Bay length: 52m
2. Ruling span: 40m
3. Phase conductor: 7/12Cu
4. Neutral conductor: Moon (7/4.75 AAC)
5. Environment: Region A – heavily vegetated area
6. Construction arrangement on poles at both ends [Construction type (separation distance)]:
 - a. Pole 1: intermediate x-arm (phase to phase: 0.5m; phase to neutral: 0.4m)
 - b. Pole 2: intermediate x-arm (phase to phase: 0.5m; phase to neutral: 0.5m)

Solution:

1. Due to high fire risk area, a mid-span separation constant k of 0.6 is selected
2. The maximum allowable sag shall be checked for phase-to-phase and phase-to-neutral:
 - a. Phase-to-phase (line-line voltage of 0.415kV)

Conductor Spacing to Avoid Midspan Clashing

Print Close

Maximum Sag/Span | Cross arm length

Pole 2 same as Pole 1

Pole 1	Pole 2
Relative Horizontal Distance: 0.5	Relative Horizontal Distance: 0.5
Relative Vertical Distance: 0	Relative Vertical Distance: 0

Maximum Allowable Conductor Sag (m): 0.69

Send Sag to Sag Tension Calc

Common Values

Max Suspension Insulator Length (m): 0

Line to Line Voltage (kV): 0.415

Midspan Separation Constant k: 0.6

This is a metric only module

Calculate Clear

Poles 'n' Wires

b. Phase-to-neutral (line-line voltage of 0.240kV)

Conductor Spacing to Avoid Midspan Clashing

Print Close

Maximum Sag/Span | Cross arm length

Pole 2 same as Pole 1

Pole 1 | Pole 2

Relative Horizontal Distance: 0.4 | 0.5

Relative Vertical Distance: 0 | 0

Maximum Allowable Conductor Sag (m): 0.56

Send Sag to Sag Tension Calc

Common Values

Max Suspension Insulator Length (m): 0

Line to Line Voltage (kV): 0.24

Midspan Separation Constant k: 0.6

This is a metric only module

Calculate Clear

Poles 'n' Wires

Based on the above, the phase-to-neutral presents the worst case scenario of allowable conductor sag.

- As dissimilar conductor is used in the same span, an assessment must be carried out to determine the one with the greater sag. Given a ruling span of 40m, the applicable tension for both conductors is 10%. Setting the conductor temperature to 50deg C under no wind condition yield the following results:

a. 7/12Cu

Sag Tension Temperature Module

Conductor: 7/12C Name: 7/12 CU

Lengths

Span Length: 52

Vertical: 0

MES: 40

Stringing Tension

%CBL: 10

Tension: 1.58

Table: 270

Temperatures

Standard: 15

No Wind: 50

Wind 1: 15

Wind 2: 15

Blowout: 50

Wind Loads

Wind 1: 500

Wind 2: 900

Blowout: 500

Loadings

No Wind: None

Wind 1: None

Wind 2: None

Calculate Tension from Sag

Sag: 0.42

Sag is under no wind, no ice loading conditions for specified Span Length and MES at No Wind temperature

Sag from Field Measurements

Units:
Distances: metres
Temperatures: °C
Wind Pressures: Pa
Tensions: kN

Description	Result
Sag @ standard temperature	0.73 m
Sag (no wind condition)	1.159 m
Sag as % of span length	2.23
Actual tension (Hor) no wind	0.995 kN
Actual tension (Hor) no wind	6.3 %CBL
Actual tension (Hor) Wind 1	2.092 kN
Actual tension (Hor) Wind 1	13.3 %CBL
Actual tension (Hor) Wind 2	2.738 kN
Actual tension (Hor) Wind 2	17.4 %CBL
Blowout	0.93 m
Transverse load 1	0.1 kN
Transverse load 2	0.19 kN

Calculate Sag from Stringing Tension

Calculate Stringing Tension from Sag

Poles 'n' Wires

b. Moon

Sag Tension Temperature Module

Conductor: MO Name 1: MOON

Lengths Span Length: 52 Vertical: 0 MES: 40		Temperatures Standard: 15 No Wind: 50 Wind 1: 15 Wind 2: 15 Blowout: 50		Wind Loads Wind 1: 500 Wind 2: 900 Blowout: 500		Loadings No Wind: None Wind 1: None Wind 2: None		Calculate Tension from Sag Sag: 0.42 Sag is under no wind, no ice loading conditions for specified Span Length and MES at No Wind temperature
Stringing Tension %CBL: 10 Tension: 1.89 Table: 220		<input type="button" value="Calculate Sag from Stringing Tension"/>		<input type="button" value="Calculate Stringing Tension from Sag"/>		<input type="button" value="Sag from Field Measurements"/>		Units: Distances: metres Temperatures: °C Wind Pressures: Pa Tensions: kN

Description	Result
Sag @ standard temperature	0.594 m
Sag (no wind condition)	1.234 m
Sag as % of span length	2.37
Actual tension (Hor) no wind	0.91 kN
Actual tension (Hor) no wind	4.8 %CBL
Actual tension (Hor) Wind 1	3.3 kN
Actual tension (Hor) Wind 1	17.5 %CBL
Actual tension (Hor) Wind 2	4.632 kN
Actual tension (Hor) Wind 2	24.5 %CBL
Blowout	1.204 m
Transverse load 1	0.19 kN
Transverse load 2	0.33 kN

Poles 'n' Wires

Any breach on the maximum allowable sags suggests there is a need for an LV spreader. Since both conditions are breached in this particular scenario, an LV spreader can be recommended:

1. Phase to phase check: 1.159m > 0.69m
2. Phase to neutral check: 1.234m > 0.56m

5. DUE DATE

This interim instruction is effective on the date it is approved.

6. WITHDRAWAL OF THIS INTERIM INSTRUCTION

This interim instruction will be withdrawn from publication 6 months after the Distribution Design Rules has been aligned and amended.